

of 100 MHz-30 GHz, the microwave attenuation is about 19 dB. The results of this study are applicable to any transparent glass coated with any thin metallic film.

#### ACKNOWLEDGMENT

The author wishes to thank H. R. Blecha, Head of the RF/EMC Evaluation Branch, for his valuable suggestions and comments.

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## Computer Program Descriptions

### NOVA (Network Optimization Via Adjoints)

**PURPOSE:** Least  $p$ th optimization of reflection coefficients and/or transducer gain of two-port microwave networks.

**LANGUAGE:** Fortran IV; 1145 cards, including comments.

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**AVAILABILITY:** ASIS/NAPS Document No. 02628. This document includes a program listing, flow charts, and user's guide including examples illustrating input data format. A deck may be obtained from J. C. Field, price furnished upon request.

**DESCRIPTION:** NOVA employs a least  $p$ th objective function [1] based on the following network responses: (1) input reflection coefficient, (2) output reflection coefficient, (3) transducer gain, or (4) a weighted combination of the first three responses. This objective function is minimized by the Fletcher-Powell algorithm [2], which was selected for its rapid, second-order convergence. The response gradients required by Fletcher-Powell are evaluated by means of adjoint network techniques [3].

Manuscript received January 1, 1975; revised May 29, 1975. See NAPS document No. 02628 for 63 pages of supplementary material. Order from ASIS/NAPS c/o Microfiche Publications, 440 Park Ave. S., New York, N. Y., 10016. Remit in advance for each NAPS accession number, \$9.95 for photocopies, \$1.50 for microfiche. Outside of the U. S. and Canada, postage is \$2.00 for a photocopy or \$.50 for a microfiche. Make checks payable to Microfiche Publications.

The allowed network configuration for NOVA is a cascade arrangement of two-port circuit elements, with the possibility of a single parallel path.

Seven basic types of circuit elements are available. They include transmission lines, open- and short-circuited shunt stubs, resistors, capacitors, and inductors. The distributed elements may be lossy or lossless, the amount of loss being specified in decibels per wavelength. Additionally, a general two-port element type is provided. This element is characterized by its measured  $S$  parameters and is useful for representing transistors or any element for which experimental data must be used. With the exception of the general element, the user may select which of the network parameters are to be varied during optimization. Since the general element is represented empirically, it is never optimized.

To avoid using excessive computer storage, a maximum of 30 network parameters and 30 frequency points were selected for NOVA. Larger networks may be accommodated by simply redimensioning the appropriate arrays. Most of the input data is in NAMELIST format to help identify each variable on a data card. The program is presently running on an IBM SYS370/145 computer and requires 42K<sub>8</sub> of core.

To illustrate program usage, an example involving the design of a 1-2-GHz amplifier is included. The goal was to achieve a flat 14-dB transducer gain over the 1-2-GHz range. The configuration of the amplifier is shown in Fig. 1, and the initial parameter values are

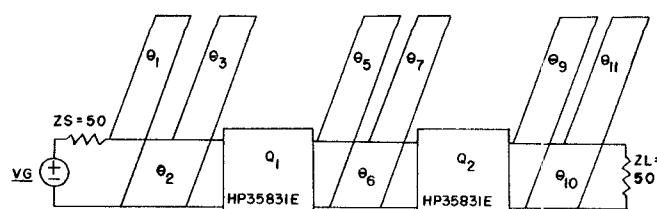


Fig. 1.

TABLE I

Element Number	Initial Electrical Length (Degrees)	Final Electrical Length (Degrees)
1	100.	49.139
2	100.	97.149
3	100.	74.658
4 (Transistor)	----	-----
5	100.	75.566
6	100.	133.061
7	100.	88.435
8 (Transistor)	----	-----
9	100.	60.446
10	100.	137.678
11	100.	63.337

Note: Initial and final element lengths for the 1-2 GHz amplifier.

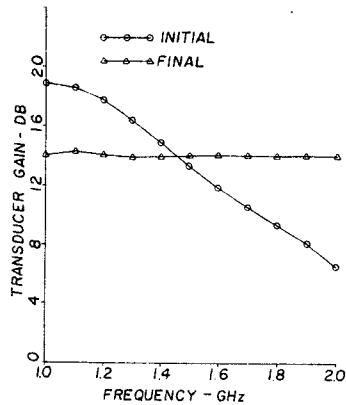


Fig. 2.

shown in Table I. All transmission line impedances were fixed at  $50 \Omega$  and only line lengths were allowed to vary. A value of  $p = 4$

was selected for the least  $p$ th objective function. The frequency points were chosen as: 1.00, 1.25, 1.50, 1.75, and 2.00 GHz. The S parameters for the HP35831E transistors were obtained from the manufacturer's specifications.

After fifteen iterations or about 122 s of computer time, the program converged to the final parameter values given in Table I. Fig. 2 shows the frequency response of both initial and final designs. In order to obtain smooth curves, the responses at additional frequency points were calculated using MECAP [4]. The optimized response is  $14 \text{ dB} + 0.315 \text{ dB}$ ,  $-0.100 \text{ dB}$  over the octave bandwidth.

#### ACKNOWLEDGMENT

The authors wish to thank J. F. Gilmore and B. W. Leake of the Raytheon Company, Wayland, Mass., for transmitting a modified version of DEMON [5], part of which is used in the analysis routine of NOVA. The subroutine MATMUL, from Calahan [6], was also used in NOVA. Finally, the authors would like to acknowledge many helpful conversations with Prof. F. H. Irons of the University of Maine.

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